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Power System Stabilizer improves standard stability using Particle Swarm Optimization.

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Abstract– Analysis of the dynamics of a singular machine connected to an endless bus power machine is presented in this study. This kind of examination requires some level of device modelling. The synchronous gadget, excitation machine, and strength gadget stabiliser are the three most popular gadget components right now. The programming tool Matlab/Simulink is used to study the performance of the device. Particle Swarm Optimization (PSO) is used to construct the energy gadget Stabilizer (PSS) in accordance with the device's performance. This is followed by simulation of the PSS design in a model and analysis of the dynamic machine response. The PSS was able to stabilise a volatile device because simulation effects without the PSS indicated poor machine response, but the PSS has progressed and stabilised an unstable device. Particle Swarm Optimization, Dynamic Stability, and Power System Stabilizer are all terms that belong in the index.

I. INTRODUCTION

One of the most important elements affecting the power system's three primary components — generation, transmission, and distribution — is power system stability. Sudden load changes, faults, and changes in generator shaft speed all have the potential to disrupt the system's stability. Stability issues have resulted in scillation that might pile up over time if left unaddressed. Because they hinder power transfer in transmission lines and stress the mechanical shaft, even low-frequency undamped oscillations are undesirable. The excitation system may be a useful tool for improving stability in the dynamic range and in the initial few cycles after a disturbance if it is designed and compensated properly. To compensate for generator rotor oscillations with dampening, a stabilising auxiliary signal is generated, and the equipment that generates it is known as a Power System Stabilizer (PSS). Controlling the generator's excitation or speed may help maintain stability. Using an Automatic Voltage Regulator AVR, the excitation may also be adjusted. PSS is now one of the most common remedies to the

AVR's instability. In addition to the automated voltage regulators system and/or the turbine controlling system of a producing unit, PSS offers extra control loops. A typical method for improving the stability of both tiny signals (steady-state) and big signals (transients), it is this one. These oscillations are commonly dampened by PSS, which is both efficient and affordable. The exciter controls the amount of current provided to the generator field winding by the AVR, which in turn regulates the voltage at the generator terminals. In most cases, it's utilised to smooth out power system tremors caused by fluctuations in load. It maintains the generator's terminal voltage at a consistent level, allowing the voltage on the load side to stay almost constant even while the load changes over time. The purpose of this article will be discussed in the next part. Section three will focus on the modelling of the whole system. In the next part, we'll go through the specifics of PSS design. Finally, implementation and simulation will be addressed in section five of this paper.

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II. MOTIVATION

The behaviour of synchronous machines following perturbation lies at the heart of the stability issue. After a change in power, machines should revert to their previous condition if possible. A new operational state is required whenever a change in load, generation, or network circumstances causes an imbalance between supply and demand. However, the synchronous machine should always stay in sync with other machines and run in parallel at the same pace. Following a system disturbance, the transient is oscillatory in nature, and these oscillations may have a major impact on power production. The amplitude of these oscillations varies depending on the perturbation. As an example of a little disturbance, consider fluctuations in load or generation that are entirely random. Any interruption, no matter how minor or huge, may disrupt the machine's synchronised functioning and cause it to lose stability. Despite this, oscillations caused by such disturbances must be dampened in order to enhance the stability of the power system. This work investigates how to address the dynamic stability of a single machine linked to an infinite bus using PSS. Stabilizing the power system of a single machine that is linked to an infinite-bus power system is the primary goal of this research.

III. SYSTEM MODELING

The system model is a crucial aspect of the design process. The synchronous machine, Automatic Voltage Regulator, and Power System Stabilizer are all modelled in this chapter.

A. Full order model

The flux connections and currents are the primary variables in the synchronous generator model's state-space form. Although these two sets are interdependent, one may be deleted and expressed in terms of the other one..

B. Single machine connected to infinite bus linear model:

Shock waves and steady-state oscillations are both present in the oscillation cycle of the generator. The transitory phase lasts for the first few cycles following a disturbance. When dynamic area is incorporated, the third-order model is simplified to a system model. As a result of this paper's concentration on small system changes, the linearized third-order model is appropriate. An infinite bus is connected to a transmission line with synchronous generator third-order resistance and reactance R. One of the presuppositions is that Everything in Xe's model is based on one assumption:

The resistance of the stator windings is not taken into account.

In the absence of saturation effects, equilibrium conditions are assumed.

The effect of the damper winding isn't considered.

Based on this assumption, a linear equation may be developed for main winding flux linkage. found: [1][2].

$$\Delta E'_q = \frac{K_3}{1 + K_3 \tau'_{d0} s} \Delta E_{FD} - \frac{K_3 K_4}{1 + K_3 \tau'_{d0} s} \Delta \delta \quad [3.1]$$

Direct-axis transient time constant FD \bar{E} is the rms value. Incremental electrical torque, on the other hand, may be calculated using the formula shown below:

$$\Delta T_e = K_1 \Delta \delta + K_2 \Delta E'_q \quad [3.2]$$

$$E'_q = E + (x_d - x'_d) I_d \quad [3.3]$$

Where \bar{E} is the stator air gap rms voltage. The synchronous generator linearized terminal voltage δ is given by:

$$\Delta V_t = K_5 \Delta \delta + K_6 \Delta E' \quad [3.4]$$

Note that the constants K_1 , K_2 , K_3 , K_4 , K_5 and K_6 are depended on system parameter and operation conditions.

In general K_1 , K_2 , K_3 and K_6 are positive, whereas K_4 is positive unless R is high. However, K_5 is positive for low and medium loading and external impedance. But if the loading and the external impedance is high K_5 will be negative. The summary of the simplified linear differential equations. of the synchronous machine are as follows:

$$\Delta E'_q = \frac{K_3}{1 + K_3 \tau'_{d0} s} \Delta E_{FD} - \frac{K_3 K_4}{1 + K_3 \tau'_{d0} s} \Delta \delta \quad [3.5]$$

$$\Delta \omega_m = \frac{1}{2H s} [\Delta T_m - \Delta T_e - D \Delta \omega_m] \quad [3.6]$$

$$\Delta \delta = \frac{\omega B}{s} \Delta \omega_m = \frac{\omega B}{s} \Delta \bar{\omega} \quad [3.7]$$

Where s is the Laplace operator.

C. Excitation system model

Synchronous generators rely heavily on their excitation systems to function properly. Strict regulation of the generator output voltage is one function of the excitation system of a synchronous generator, which is as easy as connecting the rotor windings of the generator to an external fixed dc power source. In other words, controlling the field current injected into the rotor is the goal of every synchronous machine's excitation system. By

regulating the machine's terminal voltage and keeping it constant, the generator's synchronisation is maintained via the use of field current control..

D. Representation of excitation system:

The excitation system representation is shown in Fig.3.1

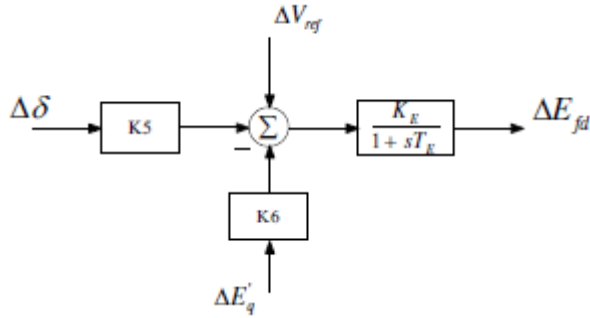


Fig. 3.1 Simple excitation system model
The linearized equation of the excitation system is given by the following equation: [1]

$$\Delta E_{fd} = \frac{K_e}{1 + sT_E} (\Delta V_{ref} - \Delta V_t) \quad [3.8]$$

E. PSS Model:

The automated voltage regulator system and/or the turbine controlling system of a producing unit both benefit from the installation of a Power System Stabilizer (PSS). These oscillations are commonly dampened by PSS, which is both efficient and affordable. Small-signal (steady state) and large-signal (transient) stability may be improved by adding additional control loops to the generator AVR [3]. PSS works in tandem with the excitation system to adjust the power angle and, as a result, dampen the oscillation. The functioning of the excitation system is critical to PSS since they operate in tandem. [4]

It is important to understand the concept of power system stabilisation, which states that the voltage controller should only be controlled by the voltage error in the steady-state (Fig.3.2). Transient states, however, have a fluctuating rotor speed due to a change in rotor angle, which causes the generator to swing and oscillate. Add an extra signal in the form of PSS that compensates for the oscillation and adds a dampening component in phase with delta[3] According to the diagram below, the PSS output (VPSS) is used as an augmenting signal for AVR control to restore the generator terminal voltage to its

original value, as shown in Fig. 3.2 below.

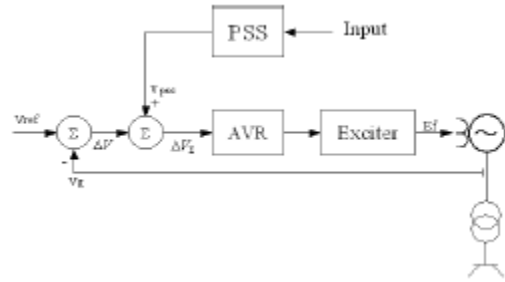


Fig.3.2: block diagram of supplementary control loop for the AVR system.

Fig. 3.3 represents the general (2 stages lead-lag power system stabilizer) structure of the PSS where VPSS is the generated based on the measured signal of the generator terminals.



Fig.3.3: lead-lag power system stabilizer.
The general equation and the used equation of the PSS is:

$$V_{PSS}(s) = \frac{sK_s T_W (1 + sT_1)(1 + sT_3)}{(1 + sT_W)(1 + sT_2)(1 + sT_4)} \text{Input}(s) \quad [3.9]$$

This particular controller structure contains a washout block, $sT_W / (1 + sT_W)$, which is used to reduce the over response of the damping during severe events. The constants T_1 , T_2 , T_3 , and T_4 should be set to provide damping over the range of frequencies at which oscillations are likely to occur.

IV. PSS DESIGN

A. Design PSS parameters using PSO:

Particle Swarm Optimization is an optimization technique which provides an evolutionary based search. This search algorithm was introduced by Dr Russ Eberhart and Dr. James Kennedy in 1995[5]. Particle Swarm Optimization (PSO) technique is inspired from birds flocking & fish schooling. Fig.4.1 shows the flow chart of PSO [6]

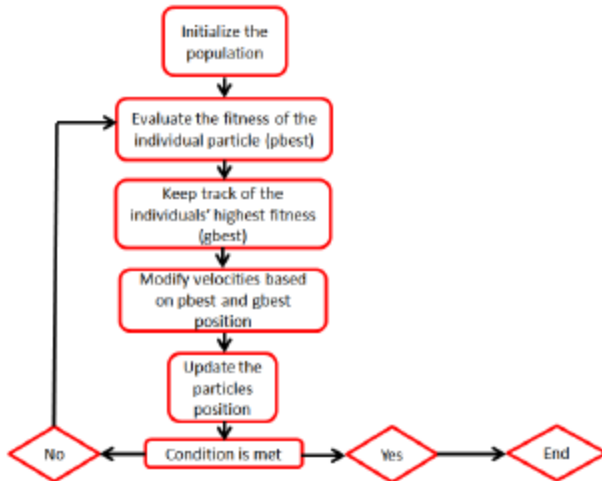


Chart of the PSO Algorithm

In PSO, the area under the curve of the speed deviation is employed as the fitness function.. When coming up with the PSS settings, PSO will strive to keep the fitness function as low as possible [4]. The following is how the fitness function is generated: initially, a Simulink simulation of the system model with a disturbance is run. After that, the speed signal is squared to remove the signal's negative component. It is then sent through an integrator to produce a measure of the fitness function's area under the curve (J). This iteration process is utilised for designing the PSS parameters that will be used in the next simulation of PSS to obtain an area under the curve that is new. As seen in Fig. 4, PSO will cycle the same procedure until it finds the smallest possible region. When one of the following circumstances is met, the search will come to an end:
 For M iterations, the fitness function's value does not change at all. M is the maximum number of iterations in which the same solution is generated.
 There is no more room for iterations.

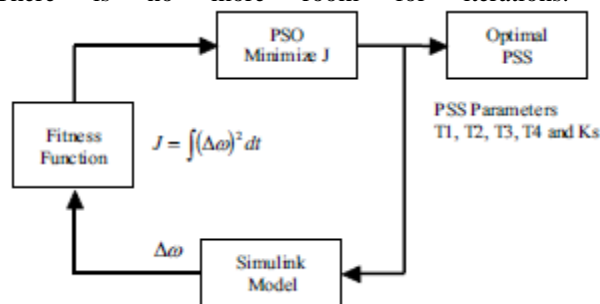


Fig.4.2: Design procedure with PSO

V. IMPLEMENTATION AND MODEL SIMULATION

A. Model Implementation

The system is simulated using MATLAB/Simulink toolbox. The models of the synchronous machine, PSS and the excitation system are linked together to form the overall system representation showing Fig 5.1.

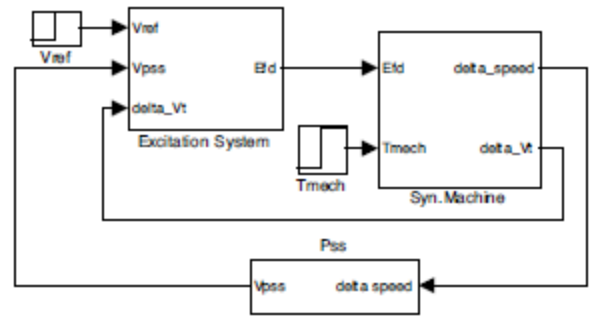


Fig.5.1: Overall system representation in Simulink

B. Synchronous machine model implementation:

Synchronous machine model consist of flux decay loop, and torque-angle loop. The model is implemented in Matlab/ Simulink as shown in Fig.5.2.

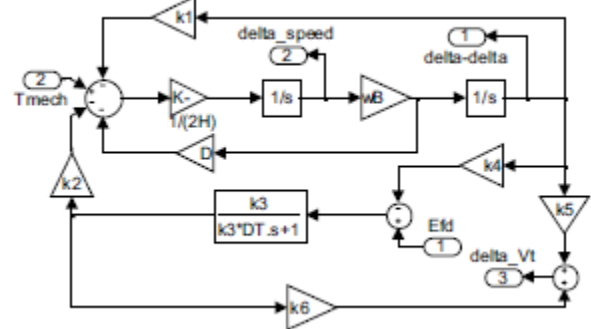


Fig.5.2: overall representation of synchronous machine

C. Excitation system implementation

Excitation system is described by equation (3.4) and equation (3.8). These equations are implemented in Matlab / Simulink as shown in Fig.5.3.

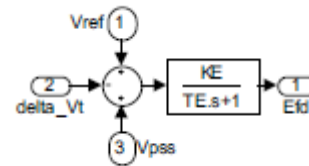


Fig.5.3: Simulink layout of excitation system

D. Power system stabilizer implementation

The PSS model presented in equation (3.9) is implemented in Matlab / Simulink as shown in Fig.5.4. The input signal to PSS is speed deviation and the output signal is VPSS which is an auxiliary signal to the excitation system.

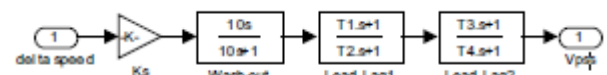


Fig.5.4: PSS implementation in Simulink

E. Case study

The performance of single machine connected to infinite bus power system is tested under a selected operating condition; the dynamic system response is analyzed considering the following variables:

1. Rotor angle deviation
2. Velocity/Speed deviation

The operating condition is listed below, where $K_5 < 0$ [6]:

Operating condition:
 $K_1 = 0.9831$ $K_2 = 1.0923$
 $K_3 = 0.3864$ $K_4 = 1.4746$
 $K_5 = -0.1103$ $K_6 = 0.4477$

$T_{do} = 5$ sec, $T_A = 0.2$ sec, $H = 6$ sec

Considering the operating condition listed above; the system response without PSS during a step load disturbance oscillates and goes out of stability.

F. Simulation Results

Table 5.1 presents a PSS parameters designed by Genetic Algorithm (GA) [4]. PSO is used in this paper to tune PSS parameters as described in the previous section. Table 5.2 presents the PSS parameters as designed by PSO.

TABLE 5.1
PSS PARAMETERS [4]

T1	T2	T3	T4	Kpss
1.4557	0.6143	1.0083	0.1005	2.1783

TABLE 5.2
PSS PARAMETERS DESIGNED BY PSO

T1	T2	T3	T4	Kpss
0.3730	0.1096	0.7910	0.0819	7.1144

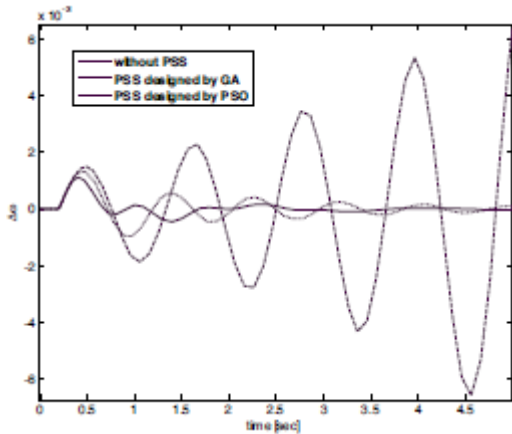


Fig 5.5: Speed deviation during 15% step load change

Figure 5.5 compare the generator speed deviation without PSS, with GA designed PSS, and with the proposed PSO

designed PSS during 15% load change. It is clear that the proposed PSS enhance the speed deviation compared to the designed PSS as published in [4].

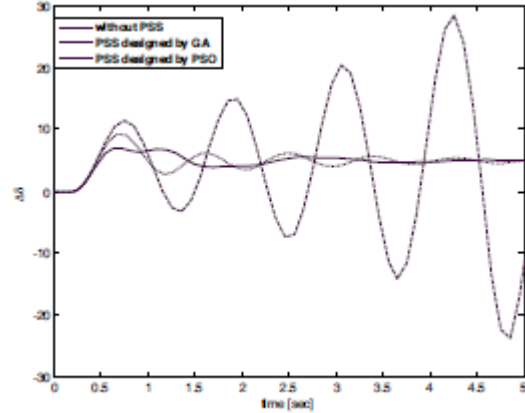


Fig 5.6: Rotor angle deviation during 15% step load change

Figure 5.6 compare the generator rotor angle deviation without PSS, with GA designed PSS, and with the proposed

PSO designed PSS during 15% load change. It is clear that the proposed PSS improve the system transient stability.

VI. CONCLUSION

Power systems are subject to several types of interruptions, such as small changes in load, which have a detrimental effect on their efficiency and may lead to system instability at times. Transmission line and shaft stress are increased when there are low-frequency oscillations, which is why they should be avoided. Adding stabilisers to AVR's prevents this from happening, and they are particularly critical in the first few cycles after a disturbance. Generator speed variation serves as the input control signal for PSS. This paper uses the single machine-infinite bus system as a case study. Investigators looked at how response was affected by the PSS. The results showed that adding PSS to the oscillatory system improved its damping and stabilised it.. The most significant contribution of this study is the creation of an ideal PSS. PSO, or particle swarm optimization, is used to build the PSS parameters. The proposed PSS design increases system responsiveness and effectively dampens oscillation when compared to a similar design through Genetic Algorithm [4].

VII. REFERENCES

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